

Investigation of glass transition behaviours in aromatic poly(amic acid) precursors with various chain rigidities by oscillating differential scanning calorimetry

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Most aromatic poly(amic acid)s, which are precursor polymers of polyimides, are thermally converted to the corresponding polyimides via imide-ring closure formation over their glass transition temperature (T_g) ranges or below. In addition, it is very difficult to remove completely solvents used in the synthesis from their cast samples, due to the formation of complexes between the solvent molecules and the orthoamic acid groups in poly(amic acid)s. For these reasons, it is not possible to measure T_g values of poly(amic acid)s with residual solvent or of poly(amic acid)s with solvent free in conventional ways. However, in the present study T_g values of several poly(amic acid)s were successfully measured as a function of the content of residual solvent by the recently developed oscillating differential scanning calorimetry: poly(*p*-phenylene biphenyltetracarboxamic acid) (BPDA-PDA), poly(*p*-phenylene pyromellitic acid) (PMDA-PDA), and poly(4,4'-oxydiphenylene biphenyltetracarboxamic acid) (BPDA-ODA) precursors. The content of residual solvent in cast poly(amic acid) samples was independently determined by proton nuclear magnetic resonance spectroscopy. By fitting the measured T_g values by a modified Gordon–Taylor equation as a function of composition, T_g values of the poly(amic acid)s in solvent free were estimated: 248.4°C for BPDA-PDA, 283.4°C for PMDA-PDA, and 184.4°C for BPDA-ODA precursor. The estimated T_g values were correlated to the calculated Kuhn statistical segments (L_K values), which are the measures of chain rigidities: 62.2 Å for BPDA-PDA, 88.7 Å for PMDA-PDA, and 41.2 Å for BPDA-ODA. That is, high chain rigidity causes higher T_g . In addition, phase diagrams of the poly(amic acid)/*N*-methyl-2-pyrrolidone solvent mixtures were constructed. The number of solvent molecules bound to the chemical repeat unit were also estimated to be 1.46–2.16 in the highly dried precursors, depending on the poly(amic acid)s. © 1998 Published by Elsevier Science Ltd. All rights reserved.

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INTRODUCTION

Aromatic polyimides are extensively used in the microelectronics industry as interdielectric layers, passivation layers and α -particle barriers, because of their excellent chemical and physical properties^{1–5}. Most aromatic polyimides are not processable due to the insolubility and high glass transition temperature (T_g) or high melting temperature (T_m), so that they are always processed in soluble precursor polymers, such as poly(amic acid)s^{6–11}, poly(amic dialkyl ester)s^{12–19}, poly(amic silyl ester)s^{20,21}, and polyisoimides^{22–24}, and then followed by either chemical or thermal imidization.

In particular, poly(amic acid)s can be simply synthesized by low-temperature polycondensation of dianhydrides and diamines in dipolar aprotic amide solvents, such as *N,N*-dimethylformamide, *N,N*-dimethylacetamide, *N*-methyl-2-pyrrolidone, and tetramethylurea^{1–11}. For this simplicity in the synthesis, poly(amic acid) precursors are widely used in the microelectronics industry. In the solution polycondensation, diamine and dianhydride reactants are weakly basic and nonprotic, respectively, and the resultant poly(amic acid) is a strong protic acid. The orthoamic acid moiety in

the poly(amic acid) is a relatively strong acid because of the electron-withdrawing effect of the orthoamide group. Thus, the orthoamic acid moieties interact strongly with the dipolar aprotic amide solvent which is a Lewis base. The strong interaction is a major source of exothermicity and of driving force in the polycondensation reaction. For these reasons, the rate of poly(amic acid) formation is generally faster in more basic and more polar aprotic solvent. The synthesized poly(amic acid) is always equilibrated with the constituent monomers^{10,11}, and thus its molecular weight and viscosity in solution vary sensitively with temperature variation and moisture contact, causing serious problems in the quality control and fabrication process. In particular, the lack of stability of poly(amic acid)s toward hydrolysis is attributed to a catalytic effect generated by the presence of the orthocarboxylic acid moiety^{19,25}, in addition to the equilibration between the precursor and the constituent monomers. Thus, poly(amic acid) solutions usually need to be stored in a refrigerator before use.

Poly(amic acid) solutions are processed in several forms, such as films, coatings, fibres and powder, and followed by drying thermally or in vacuum. Then, the dried poly(amic acid)s in various forms are converted chemically or thermally to the corresponding polyimides. The chemical imidization of poly(amic acid)s is commonly performed

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with the aid of acid anhydride dehydrating agents with tertiary amines via cyclodehydration^{26,27}. The chemically imidized products are washed and finally dried thermally or in vacuum to remove residual solvents. On the other hand, the thermal imidization is carried out by heat-treatment up to 200–400°C, depending upon the thermal stability of the resultant polyimide^{10,28–37}. In general, the imidization kinetic depends upon the backbone structure of precursor, solvent, temperature and catalyst.

In fact, the thermal imidization of poly(amic acid)s has been investigated in detail by a number of research groups^{28–37}, despite the nature of complexity. However, the glass transition of poly(amic acid)s has been rarely examined. There are two main difficulties in direct measurements of T_g values in poly(amic acid)s with solvent free: first, poly(amic acid)s form complexes with dipolar aprotic solvents through strong interactions between the orthoamic acid groups of the precursor polymer and the basic solvent molecules, so that it is very difficult to remove all solvent molecules from cast poly(amic acid) specimens by drying. Each orthoamic acid group of poly(amic acid)s in *N*-methyl-2-pyrrolidone (NMP) is known to complex with one or two NMP molecules³³. For this complex formation, dried poly(amic acid) specimens still contain typically >20 wt.% of NMP, depending on the drying conditions^{31–38}. The residual solvent significantly reduces T_g values of poly(amic acid)s, and furthermore, influences severely the imidization kinetic of poly(amic acid)s. Second, aromatic poly(amic acid)s exhibit relatively high T_g due to their relatively high chain rigidities. Over the T_g range or below, they start to imidize to the corresponding polyimides. In general, most poly(amic acid)s in dried specimens initiate to imidize about 130°C, and their imidizations are accelerated with increasing temperature^{28–32}. That is, the glass transitions of most aromatic poly(amic acid)s are overlapped with or higher than their imidization temperatures. Despite these difficult circumstances, measurements of glass transition have been attempted for numerous aromatic poly(amic acid)s. However, the T_g values of only a few poly(amic acid)s have been measured which were lower than 130°C, the onset temperature of imidization^{34,39}. For example, poly(4,4'-oxydiphenylene 3,3',4,4'-oxydiphthalamic acid) in specimens was measured to have a T_g of 125°C by differential scanning calorimetry (d.s.c.)³⁹. Also, poly(4,4'-oxydiphenylene-*co-p*-phenylene benzophenonetetracarboxamic acid) was characterized to exhibit a T_g of 125°C in dynamic mechanical thermal spectra³⁴. For these poly(amic acid)s, the specimens still contained some amounts of residual solvent, so that the measured T_g values are not the true glass transition temperatures.

In the present study, several poly(amic acid)s with various chain rigidities were synthesized in NMP solvent by conventional polycondensation reaction of aromatic dianhydrides and diamines: poly(*p*-phenylene biphenyl-tetracarboxamic acid), poly(*p*-phenylene pyromellitic acid), and poly(4,4'-oxydiphenylene biphenyltetracarboxamic acid). The synthesized poly(amic acid) solutions were cast on glass slides and softbaked, followed by further drying in vacuum. T_g values of the dried precursor samples were attempted to measure, using oscillating differential scanning calorimetry (O-d.s.c.) technique^{40–45}. In addition, amounts of residual NMP solvent in the precursor samples were determined by nuclear magnetic resonance (n.m.r.) spectroscopy. The T_g values of the poly(amic acid)s in solvent free were estimated from the best fitting of T_g values measured with varying residual NMP content by a modified

Gordon–Taylor equation^{46,47}. The true T_g values estimated were interpreted with considering the chain rigidity of poly(amic acid) precursors.

EXPERIMENTAL

Materials and characterization

Aromatic dianhydrides and diamines used in this study were supplied by Aldrich Chemical Company and Chriskev Company: pyromellitic dianhydride (PMDA), biphenyl-tetracarboxylic dianhydride (BPDA), *p*-phenylene diamine (PDA), and 4,4'-oxydiphenylene diamine (ODA). All monomers were purified by sublimation under reduced pressure and then used for polymerization.

Poly(*p*-phenylene biphenyltetracarboxamic acid) (BPDA-PDA) was prepared in a glove box filled with dry nitrogen gas by slowly adding the sublimed BPDA to the purified PDA in dry *N*-methyl-2-pyrrolidone (NMP) with a boiling point of 202°C and a melting point of –23.6°C. Once the dianhydride addition was completed, the reaction flask was capped tightly and stirring was continued for 2 days to make the polymerization mixture completely homogeneous. Other poly(amic acid)s were prepared in the same manner as BPDA-PDA was synthesized: BPDA-ODA and PMDA-PDA precursors (see *Figure 1*). The solid content of the precursor solutions was 10–15 wt%. The precursor solutions were filtered with silver metal membranes of 1.0 μm pore size, tightly sealed, and stored in a refrigerator before use.

In the synthesis of poly(amic acid)s, molecular weights were attempted to be controlled by stoichiometric imbalance of the monomers using the diamine in small excess. For the synthesized poly(amic acid)s, intrinsic viscosity [η] measurements were carried out in NMP at 25.0°C using an Ubbelohde suspended level capillary viscometer, as described in the literature^{48,49}. Here, in order to minimize polyelectrolyte effect in the viscosity measurement, NMP was purified by distillation over phosphorus pentoxide (P₂O₅) under reduced pressure and further treated with 0.02 M P₂O₅, followed by filtration before use^{48,49}. All the solutions were filtered through 0.5 μm Fluoropore filters (Millipore) before measurement. For a given poly(amic acid), the relative and specific viscosities were measured at four different concentrations over the range of 0.10–0.60 g/dl, and the [η] value was determined by extrapolation of the reduced and inherent viscosities to infinite dilution. The [η] was determined to be 0.683 dl/g for the BPDA-PDA precursor, 0.690 dl/g for the BPDA-ODA precursor, and 0.538 dl/g for the PMDA-PDA precursor.

Poly(amic acid) solutions were cast on precleaned glass slides and softbaked on a hotplate of 80°C for 10–60 min. Some of the films softbaked for 1 h were further dried in a vacuum oven at 50°C for various times: 2, 4 and 7 days. The contents of residual NMP in these precursor films were determined by proton nuclear magnetic resonance (n.m.r.) spectroscopy as described in the following: small pieces of a dried precursor film were dissolved in dimethyl-*d*₆ sulphoxide (DMSO-*d*₆), and the residual NMP and precursor polymer in the solution were characterized using a Bruker NMR spectrometer (Model: Aspect 300 MHz) with a proton probe. Then, the amount of NMP in weight percent was estimated from the measured n.m.r. spectra.

Glass transition and imidization temperatures of the dried precursor samples were measured in either ordinary mode or oscillating mode over –60–400°C under dry nitrogen gas flow using a Seiko oscillating differential scanning

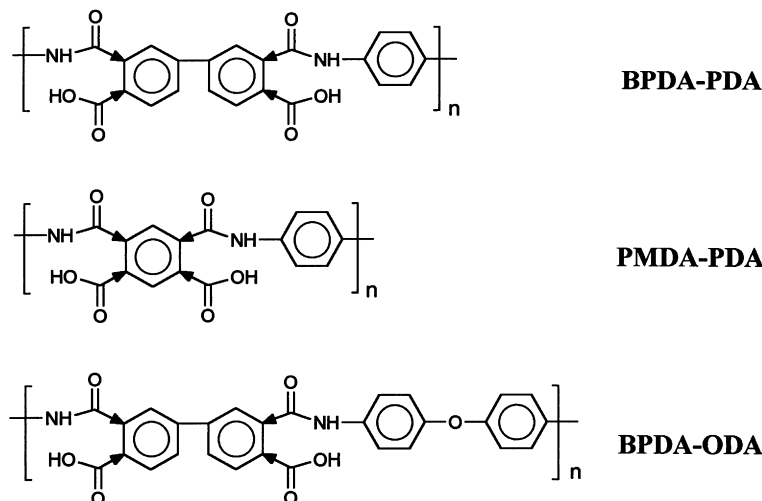


Figure 1 Chemical structures of aromatic poly(amic acids) synthesized in this study

calorimeter (Model: ODS-220CU). During the measurements, dry nitrogen gas was purged with a flow rate of 80 cc/min. Temperature calibration was carried out using indium and tin and enthalpy calibration using indium. In the scanning run, a sample of 2 mg was used. A heating rate of 10.0 K/min was employed. An oscillating amplitude of 10.0°C and an oscillating frequency of 0.02 Hz were used, respectively.

Oscillating differential scanning calorimetry

The oscillating differential scanning calorimetry (O-d.s.c.) technique is briefly described here. In contrast to the ordinary differential scanning calorimetry, in which the input signal consists of only a linear component, the input signal $T(t)$ of O-d.s.c. in temperature is composed of linear and oscillating components as described in the following^{40–45}:

$$T(t) = T_o + T_{\text{ramp}}(t) + T_{\text{os}}(t) \quad (1)$$

$$= T_o + Bt - A \sin(2\pi ft) \quad (2)$$

where T_o , $T_{\text{ramp}} (=Bt)$ and $T_{\text{os}} [= -A \sin(2\pi ft)]$ are the start temperature, the linear heating component, and the oscillating heating component, respectively. A and B are the oscillating amplitude and the heating rate, respectively, whereas t and f are the time and the oscillating frequency, respectively. For the O-d.s.c. used in this study, the oscillating frequency f is in the range of 0.01–0.1 Hz.

The output signal in the O-d.s.c. is also composed of linear and oscillating components. Thus, the output signal $Y(t)$ (namely, total heat flow) can be separated into two signal components in the following:

$$Y(t) = Y_{\text{ramp}}(t) + Y_{\text{os}}(t) \quad (3)$$

where $Y_{\text{ramp}}(t)$ and $Y_{\text{os}}(t)$ are the linear and the oscillating d.s.c. signal components, respectively. In addition, the total heat flow can be also expressed by the sum of the specific heat flow $Y_{\text{sp}}(t)$ and the kinetic heat flow $Y_{\text{k}}(t)$. Thus, equation (3) can be rewritten below:

$$Y(t) = Y_{\text{sp}}(t) + Y_{\text{k}}(t) \quad (4)$$

Here, the specific heat flow appears in thermally reversible phenomena such as glass transition and melting transition. On the other hand, the kinetic heat flow appears in thermally irreversible phenomena such as chemical reaction, evaporation, and decomposition.

The specific heat flow component $Y_{\text{sp}}(t)$ in equation (4) can be expressed by a function of the temperature $T(t)$ of equation (1) and the heat capacity C_p , whereas the oscillating d.s.c. signal component $Y_{\text{os}}(t)$ in equation (3) can be described by a function of the oscillating temperature $T_{\text{os}}(t)$ in equation (1) and C_p :

$$Y_{\text{sp}}(t) = -C_p \frac{dT(t)}{dt} \quad (5)$$

and

$$Y_{\text{os}}(t) = C_p \frac{dT_{\text{os}}(t)}{dt} \quad (6)$$

Taking into account equation (2) and equation (6), $Y_{\text{sp}}(t)$ in equation (5) can be obtained as the following form:

$$Y_{\text{sp}}(t) = \left[\frac{B}{2\pi f} - A \cos(2\pi ft) \right] \left[\frac{Y_{\text{os}}(t)}{A \cos(2\pi ft)} \right] \quad (7)$$

Here,

$$A \cos(2\pi ft) = A \sin \left\{ 2\pi f \left(t - \frac{1}{4f} \right) \right\} \quad (8)$$

$$= T_{\text{os}} \left(t - \frac{1}{4f} \right) \quad (9)$$

By taking into account equation (9), the specific heat flow component $Y_{\text{sp}}(t)$ is finally expressed below:

$$Y_{\text{sp}}(t) = \left[\frac{B}{2\pi f} - T_{\text{os}} \left(t - \frac{1}{4f} \right) \right] \left[\frac{Y_{\text{os}}(t)}{T_{\text{os}} \left(t - \frac{1}{4f} \right)} \right] \quad (10)$$

Thus, the kinetic heat flow component $Y_{\text{k}}(t)$ can be obtained by subtracting the specific heat flow component $Y_{\text{sp}}(t)$ from the total heat flow $Y(t)$:

$$Y_{\text{k}}(t) = Y(t) - Y_{\text{sp}}(t) \quad (11)$$

As described above, the O-d.s.c. technique has several advantages, compared to the ordinary d.s.c.. The first advantage is the effective separation of specific heat flow, that appears in thermally reversible phenomena such as glass and melting transitions, from the kinetic heat flow that reveals in thermally irreversible phenomena such as chemical reaction, evaporation, and decomposition. The second is

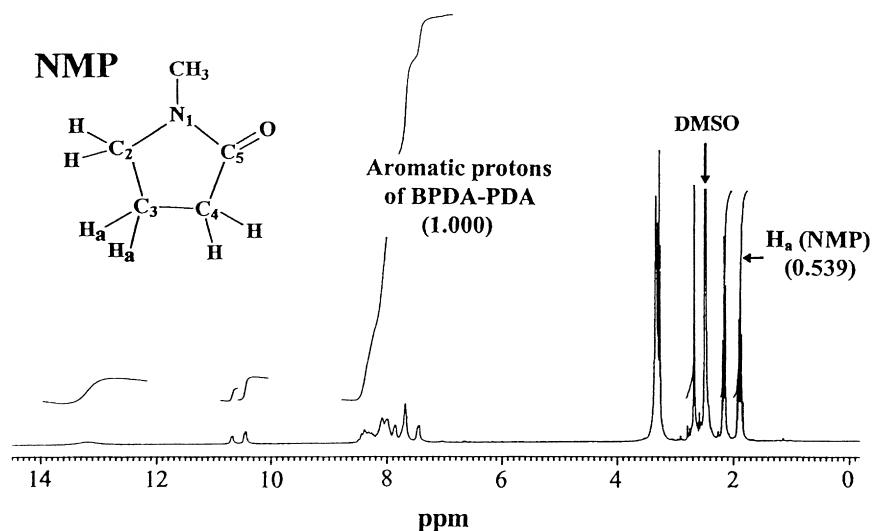


Figure 2 ^1H n.m.r. spectrum of a BPDA-PDA precursor sample softbaked at 80°C for 1 h, which was dissolved in dimethyl- d_6 sulphoxide (DMSO- d_6)

Table 1 Compositions, glass transition (or melting) temperatures (T_g or T_m values), and imidization temperatures (T_i values) of BPDA-PDA precursor samples dried under various conditions

Precursor sample	Drying condition	Composition ^a		T_g (or T_m) ($^\circ\text{C}$)	T_i^b ($^\circ\text{C}$)
		NMP (wt.%)	Precursor (wt.%)		
Sample #1	(NMP itself)	100	0	-23.6^c	—
#2	(Precursor solution itself)	88.3	11.7	-29.5^c	—
#3	$80^\circ\text{C}/10$ min	78.1	21.9	-29.2^c	—
#4	$80^\circ\text{C}/20$ min	66.4	33.6	-33.6^c	—
#5	$80^\circ\text{C}/1$ h	39.9	60.1	39.3^d	138.7
#6	$80^\circ\text{C}/1$ h + $50^\circ\text{C}/2$ day (in vacuum)	34.6	65.4	85.5^d	139.0
#7	$80^\circ\text{C}/1$ h + $50^\circ\text{C}/4$ day (in vacuum)	30.5	69.5	117.2^d	146.9
#8	$80^\circ\text{C}/1$ h + $50^\circ\text{C}/7$ day (in vacuum)	26.5	73.5	133.0^d	154.7

^a Measured by proton n.m.r. spectroscopy

^b Onset temperature of imidization measured by O-d.s.c.

^c T_m measured from the peak maximum of NMP melting in ordinary differential scanning calorimetry (d.s.c.) run

^d T_g measured from the onset of glass transition in oscillating differential scanning calorimetry (O-d.s.c.) run

the precise measurement of very weak glass transition. The other is the precise measurement of specific heat changes (ΔC_p values) in glass and melting transitions.

RESULTS AND DISCUSSION

N.m.r. spectroscopic determination of residual solvent

In general, the glass transition of a polymer in films prepared by solution casting and subsequent drying is strongly dependent upon the amount of residual solvent. As mentioned above, poly(amic acid)s, which were synthesized in NMP solvent, form complexes with NMP molecules via strong interaction between the orthocarboxylic acid group of the precursor and the tertiary amino group of the NMP, so that NMP solvent could not be removed completely from the cast samples by drying process. The residual NMP solvent affects severely the glass transition of poly(amic acid)s. Therefore, in this study the amounts of residual NMP solvent in precursor samples dried at various conditions were measured by proton n.m.r. spectroscopy and correlated to the T_g values determined independently by O-d.s.c. technique.

For a BPDA-PDA poly(amic acid) sample softbaked at 80°C for 1 h, its tiny pieces were dissolved in DMSO- d_6 and characterized by proton n.m.r. spectroscopy. The measured

n.m.r. spectrum is illustrated in *Figure 2*. The two protons (2H_a) of the carbon-3 (C_3) in the five-membered ring of NMP appeared at $\delta = 1.75\text{--}2.05$ ppm, whereas the 10 aromatic protons in the repeat unit of BPDA-PDA poly(amic acid) showed at $\delta = 7.3\text{--}8.6$ ppm as multiple peaks. The amount of NMP solvent in weight fraction (W_s) was estimated from the integrations of these peaks in the following:

$$W_s = \frac{\left[\frac{A_{2\text{H}_a}}{N_{2\text{H}_a}} \right] [M_{\text{NMP}}]}{\left[\frac{A_{2\text{H}_a}}{N_{2\text{H}_a}} \right] [M_{\text{NMP}}] + \left[\frac{A_{\text{ar}}}{N_{\text{ar}}} \right] [M_p]} \quad (12)$$

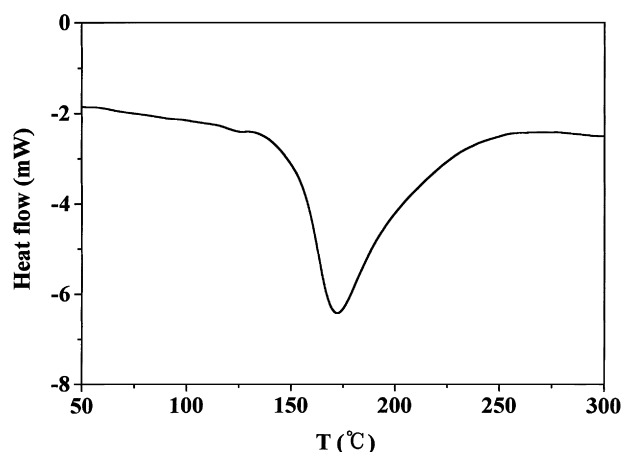
where $A_{2\text{H}_a}$, $N_{2\text{H}_a}$, and M_{NMP} are the integration of the two proton signals, the number of H_a protons, and the molecular weight of NMP, respectively, and A_{ar} , N_{ar} , and M_p are the total integration of the aromatic proton signals, the number of the aromatic protons in a chemical repeat unit, and the molecular weight of the chemical repeat unit in the precursor, respectively. The NMP content in the dried film was determined to be 39.9 wt.%. Thus, the content of the precursor polymer (that is, W_p in percentage) was 60.1 wt.%. For precursor samples dried at the other conditions, NMP and polymer contents were determined in the same manner.

Table 2 Compositions, glass transition temperatures (T_g values), and imidization temperatures (T_i values) of PMDA-PDA precursor samples dried under various conditions

Precursor sample	Drying condition	Composition ^a		T_g^b (°C)	T_i^c (°C)
		NMP (wt.%)	Precursor (wt.%)		
Sample #1	80°C/1 h	52.9	47.1	26.2	123.0
#2	80°C/1 h + 50°C/ 2 day (in vacuum)	44.9	55.1	88.2	125.4
#3	80°C/1 h + 50°C/ 4 day (in vacuum)	42.7	57.3	108.6	128.9
#4	80°C/1 h + 50°C/ 7 day (in vacuum)	39.6	60.4	112.8	131.5

^aMeasured by proton n.m.r. spectroscopy^b T_g measured from the onset of glass transition in oscillating differential scanning calorimetry (O-d.s.c.)^cOnset temperature of imidization measured by O-d.s.c.**Table 3** Compositions, glass transition temperatures (T_g values), and imidization temperatures (T_i values) of BPDA-ODA precursor samples dried under various conditions

Precursor sample	Drying condition	Composition ^a		T_g^b (°C)	T_i^c (°C)
		NMP (wt.%)	Precursor (wt.%)		
Sample #1	80°C/1 h	41.6	58.4	31.2	131.3
#2	80°C/1 h + 50°C/ 2 day (in vacuum)	30.0	70.0	102.0	136.1
#3	80°C/1 h + 50°C/ 4 day (in vacuum)	26.2	73.8	113.8	140.3
#4	80°C/1 h + 50°C/ 7 day (in vacuum)	25.8	74.2	115.1	149.3

^aMeasured by proton n.m.r. spectroscopy^b T_g measured from the onset of glass transition in oscillating differential scanning calorimetry (O-d.s.c.)^cOnset temperature of imidization measured by O-d.s.c.**Figure 3** The ordinary d.s.c. thermogram of a BPDA-PDA precursor sample containing 26.5 wt.% residual NMP solvent. A heating rate of 10.0 K/min was employed

As summarized in *Table 1*, the precursor solution contained 88.3 wt.% NMP, and the dried precursor samples had 26.5–78.1 wt.% NMP, depending on the drying conditions.

Similar characterization of residual NMP was performed for PMDA-PDA and BPDA-ODA precursor samples dried at various conditions. The results are listed in *Tables 2* and *3*, respectively. For PMDA-PDA precursor, the sample dried at 80°C/1 h contained 52.9 wt.% NMP, and the other samples had 39.6–44.9 wt.% NMP, depending on the drying conditions. For BPDA-ODA precursor, the sample

dried at 80°C/1 h contained 41.6 wt.% NMP, and the other samples had 25.8–30.0 wt.% NMP, depending on the drying conditions.

Overall, the content of residual NMP in the dried precursor sample was dependent first on the initial concentration of the precursor solution and then reduced by drying: longer drying time gave lower residual NMP. The lowest NMP content was 26.5 wt.% for the BPDA-PDA precursor sample, 39.6 wt.% for the PMDA-PDA precursor, and 25.8 wt.% for the BPDA-ODA precursor: here, all the precursor samples were dried for 7 days at 50°C in vacuum. For these highly dried precursor samples, all the residual NMP molecules are assumed to participate in forming complexes with the orthoamic acid groups of the precursors and then the number of NMP molecules bound to the repeat units of the precursors can be estimated from the contents of residual NMP measured by n.m.r. spectroscopy. The number of the NMP molecules bound per chemical repeat unit of precursor is calculated to be 1.4 for the BPDA-PDA, 2.1 for the PMDA-PDA, and 1.7 for the BPDA-ODA precursor. These are in good agreement with the results published previously in the literature³³.

O-d.s.c. measurements

A BPDA-PDA precursor sample with a residual NMP of 26.5 wt.% was characterized by ordinary and oscillating d.s.c. techniques. From the ordinary d.s.c. thermogram in *Figure 3*, the heat flow curve of glass transition is not recognizable because the endothermic heat flow due to the imidization is very dominant over the temperature range of 115–280°C. Thus, only the imidization temperature of the precursor sample can be estimated from the ordinary d.s.c. thermogram. In contrast, *Figure 4* shows the oscillating input temperature signals as well as the oscillating d.s.c. output signals as a function of time. The O-d.s.c. thermogram can be nicely separated into two parts, the specific heat flow and the kinetic heat flow, by equation (10) and equation (11) described in the Experimental Section. The separated specific and kinetic heat flows are plotted in *Figure 5* as a function of temperature. The specific heat flow curve reveals clearly glass transition over 115–165°C. From this thermogram, T_g was determined to be 133.0°C for the dried precursor sample: here, T_g is defined as the onset temperature of glass transition in the specific heat flow. On the other hand, the kinetic heat signal curve shows a broad, big endothermic heat flow peak which results from the imidization reaction and the removal of the reaction byproduct (i.e. water) and residual solvent. The onset temperature of imidization (T_i) in the dried film was estimated to be 148.1°C.

The O-d.s.c. measurement was carried out for the other BPDA-PDA precursor samples dried at various conditions. For the precursor samples with a residual NMP of <50 wt.%, the separated specific heat and kinetic heat flow curves are illustrated in *Figures 6* and *7*, respectively, and compared with those of the sample described above, respectively. Both T_g and T_i of each sample were estimated from the heat flow curves and listed in *Table 1*. As the content of residual NMP in the precursor sample reduced to 26.5 wt.% from 39.9 wt.%, T_g increased to 133.0 from 39.3°C and T_i also increased to 154.7°C from 138.7°C. Overall, the residual NMP in the precursor sample caused the lowering of both glass transition and imidization temperatures. However, the effect of residual NMP is relatively much higher in the T_g than the T_i .

The O-d.s.c. investigation was extended to the precursor

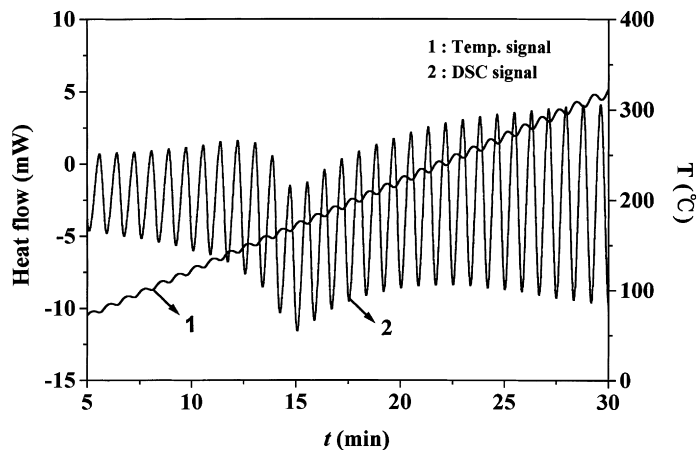


Figure 4 The input temperature signal and out O-d.s.c. signal of a BPDA-PDA precursor sample containing 26.5 wt.% residual NMP solvent. A heating rate of 10.0 K/min was employed. The temperature amplitude and frequency used in the oscillation were 10.0°C and 0.02 Hz, respectively

samples which contained >50 wt.% NMP, including NMP itself as well as the precursor solution itself, with a concentration of 11.7 wt.%. These samples exhibited glass transition or melting transition at a temperature region much lower than their imidization temperature, so that measurements were carried out in the ordinary mode. The results are listed in *Table 1*. The melting point (T_m) of the pure NMP was -23.6°C : Here, T_m is defined as the temperature of the peak maximum of NMP melting in the ordinary d.s.c. signal. For the precursor samples, including the precursor solution, the T_m of NMP component was depressed, depending on the content of precursor polymer. T_m was measured to be -29.5°C for the precursor solution itself with 11.7 wt.% precursor, -29.2°C for the sample with 21.9 wt.% precursor, and -33.6°C for the sample with 33.6 wt.% precursor.

In addition, from these T_g (or T_m) data with varying compositions, it has been attempted to make a phase diagram for the BPDA-PDA precursor/NMP mixture. The measured T_g values (or T_m values) are plotted in *Figure 8*. The T_m in the mixture with the major NMP component decreases linearly with increasing precursor content, whereas the T_g in the mixture with the major precursor component decreases convexly with increasing NMP content. They are extrapolated to meet at a composition of 49.2 wt.% NMP and 50.8 wt.% precursor. In particular, the solid curve line at a concentration of >50.8 wt.% precursor is a curve fitted by a modified Gordon–Taylor equation. This will be described in detail below.

Both PMDA-PDA and BPDA-ODA precursors in the dried sample were characterized by O-d.s.c. in the same manner as the BPDA-PDA precursor samples were investigated. For all the O-d.s.c. thermograms, the specific heat flow parts were separated from the kinetic heat flow parts. Both T_g and T_i values, which were estimated from the separated specific and kinetic heat flow curves, respectively, are summarized in *Tables 2* and *3*. For PMDA-PDA samples, as the content of residual NMP varied from 52.9 to 39.6 wt.%, T_g increased from 26.2 to 112.8°C, whereas T_i also increased from 123.0 to 131.5°C. Similar dependency of residual NMP in both T_g and T_i was observed for the BPDA-ODA precursor sample. T_g in the precursor sample varied in the range of 31.2–115.1°C and T_i varied over the range of 131.3–149.3°C, depending on the content of NMP. Overall, for the precursor samples, higher NMP

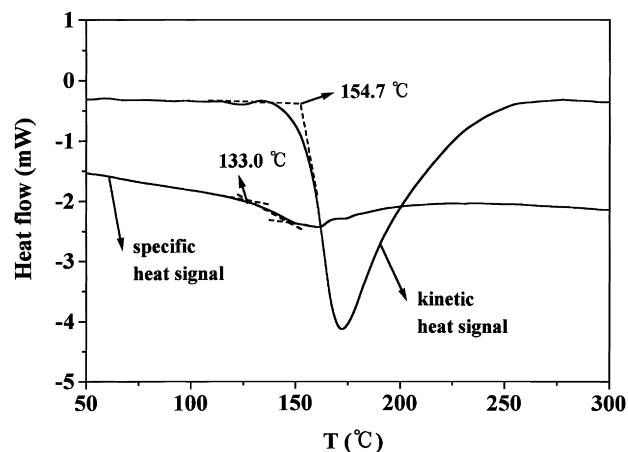


Figure 5 The signals of specific and kinetic heat flow component separated from the O-d.s.c. thermogram in *Figure 4*, which was obtained for a BPDA-PDA precursor sample containing 26.5 wt.% residual NMP solvent

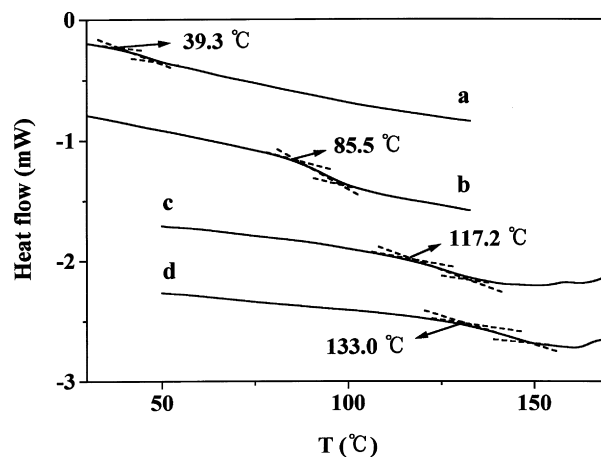


Figure 6 The signals of specific heat flow component separated from O-d.s.c. thermograms obtained for BPDA-PDA precursor samples containing various amounts of residual NMP: (a) 39.9 wt.% NMP; (b) 34.6 wt.%; (c) 30.5 wt.%; (d) 26.5 wt.%. A heating rate of 10.0 K/min was employed. The temperature amplitude and frequency used in the oscillation were 10.0°C and 0.02 Hz, respectively

content caused lower T_g and T_i , as observed in the BPDA-PDA precursor sample.

Estimation of T_g values of poly(amic acid) precursors with solvent free

From the T_g values measured from the precursor samples contained residual NMP, it was attempted in this section to estimate true T_g values of the poly(amic acid) precursors, namely, T_g values of the precursors in solvent free. This is possible by a reasonable theoretical analysis of the measured T_g values.

T_g versus composition in miscible binary blends of polymers and plasticizers was reported to have many variations^{46–57}. For polymer blends miscible over the entire range of composition, three generalized T_g -composition curves are reported: (i) the linear relationship^{50,51}; (ii) the concave deviation from the linearity^{52–54}; and (iii) the convex deviation from the linearity^{55–57}. Both the linear and concave relationships indicate the miscibility results

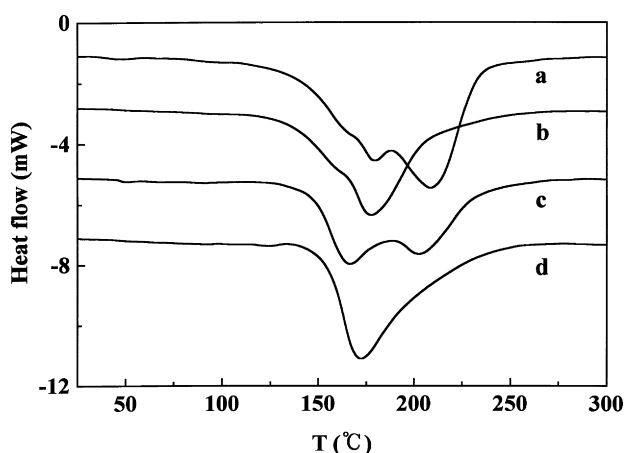


Figure 7 The signals of kinetic heat flow component separated from O.d.s.c. thermograms obtained for BPDA-PDA precursor samples containing various amounts of residual NMP: (a) 39.9 wt.% NMP; (b) 34.6 wt.%; (c) 30.5 wt.%; (d) 26.5 wt.%. A heating rate of 10.0 K/min was employed. The temperature amplitude and frequency used in the oscillation were 10.0°C and 0.02 Hz, respectively

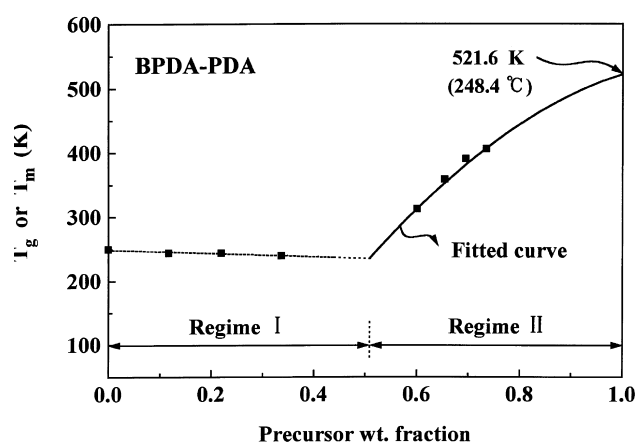


Figure 8 The variation of glass transition temperature (T_g) or melting point (T_m) of BPDA-PDA precursor/NMP mixture as a function of precursor weight fraction. The ■ symbols denote the measured phase transition temperatures. The solid curve is the curve fitted by a modified Gordon–Taylor equation, equation (18) from the T_g data measured in the regime II

from the intermolecular interaction based on mainly van der Waals attraction between the blend components. On the other hand, the convex relationship is known to result from strong intermolecular interactions, such as hydrogen bonding, acid–base interaction, and charge complexation, between the blend components. These T_g variations with composition were attempted to be described by several theoretical and empirical expressions, such as the Fox⁵², Gordon–Taylor⁵³, Kelley–Bueche⁵⁴, Gibbs–Dimarzio⁵⁸, Kanig⁵⁹, Wood⁶⁰, modified Fox⁶¹, modified Gibbs–Dimarzio⁶², and modified Gordon–Taylor^{46,47}, equations: here, it is noted that some of these equations have been originally developed to illustrate T_g variations in copolymers.

In particular, convex T_g behaviours with composition observed in miscible polymer–polymer blend systems with strong interactions between the components^{56,57} have been successfully described by a modified Gordon–Taylor equation, that was introduced for copolymer systems by Jenckel *et al.*⁴⁶ and Uemastu *et al.*⁴⁷ For example, the convex T_g behaviour in the blend of poly(vinyl nitrate) and poly(vinyl acetate) obeyed the modified Gordon–Taylor expression⁵⁷. The modified Gordon–Taylor expression was adapted in the present study in order to illustrate convex T_g variations with composition in the poly(amic acid)s contained residual NMP solvent via strong acid–base complexation between the orthoamic acid group of the polymers and the secondary amino group of the NMP molecules and, furthermore, to estimate their true T_g values in residual solvent free.

The modified Gordon–Taylor equation can be expressed in the following^{46–57}:

$$T_g = \frac{\Delta\alpha_s T_{g,s} W_s + \Delta\alpha_p T_{g,p} W_p}{\Delta\alpha_s W_s + \Delta\alpha_p W_p} + \frac{\Delta k W_s W_p}{\Delta\alpha_s W_s + \Delta\alpha_p W_p} \quad (13)$$

where

$$\Delta\alpha_i = \alpha_{r,i} - \alpha_{g,i} \quad (14)$$

and

$$\Delta k = k_g - k_r \quad (15)$$

Here, T_g is the glass transition temperature of a mixture containing the weight fractions, W_s and W_p , of two components (i.e. NMP solvent, s and precursor polymer, p) in which glass transition temperatures are $T_{g,s}$ (that is, melting point (T_m) of NMP) and $T_{g,p}$, respectively. $\Delta\alpha_i$ is the difference between the volume expansion coefficients, $\alpha_{r,i}$ and $\alpha_{g,i}$, of the component i in the rubbery (or liquid) and glassy states. k_g and k_r are the parameters representing the volume changes on mixing of two components in a mixture as expressed in the following:

$$V_g = V_{g,s} W_s + V_{g,p} W_p + k_g W_s W_p \quad (16)$$

and

$$V_r = V_{r,s} W_s + V_{r,p} W_p + k_r W_s W_p \quad (17)$$

where V_g and V_r are the specific volumes of a mixture in the glassy and rubbery (or liquid) states, respectively. $V_{g,i}$ and $V_{r,i}$ are the specific volumes of the component i in the glassy and rubbery (or liquid) states, respectively. The changes in the specific volumes with the temperature are assumed to be linear.

In this study, poly(amic acid) precursors contained residual NMP solvent were observed to exhibit a *two-regime* behaviour in the phase transition with composition. For the BPDA-PDA precursor/NMP mixture shown in *Figure 8*, in

Table 4 Constants used in estimating the Δk of BPDA-PDA poly(amic acid)

Constant	
$\Delta\alpha_s$	3.27×10^{-4} cc/g-K
$\Delta\alpha_p$	2.69×10^{-4} cc/g-K
$\Delta\alpha_1$	2.92×10^{-4} cc/g-K
$\Delta\alpha_3$	2.84×10^{-4} cc/g-K
ΔT_2	9.6 K
$\Delta T_{2'}$	12.4 K
$W_3 - W_1$	0.143

Table 5 Constants used to estimate T_g values of poly(amic acid)s in solvent free^a

Precursor	V_w (cc/g)	$\Delta\alpha$ (cc/g-K)	Δk	W_c	T_g (°C)
BPDA-PDA	0.488	2.69×10^{-4}	$0.106 \times (1 - W_c)$	0.521	248.4
PMDA-PDA	0.507	2.79×10^{-4}	$0.106 \times (1 - W_c)$	0.404	283.4
BPDA-ODA	0.497	2.74×10^{-4}	$0.106 \times (1 - W_c)$	0.505	184.4

^aThe V_w and $\Delta\alpha$ of the pure NMP solvent were calculated to be 0.595 cc/g and 3.27×10^{-4} cc/g-K, respectively

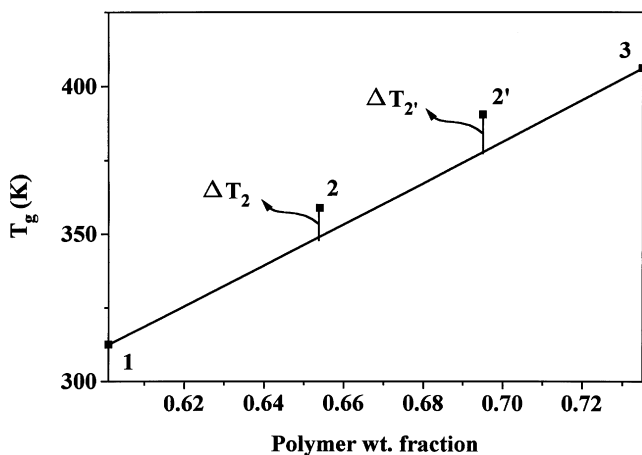


Figure 9 The variation of glass transition temperature (T_g) of BPDA-PDA precursor/NMP mixture in the *regime II* as a function of precursor weight fraction: The \blacksquare symbols, which are denoted by 1, 2, 2', and 3, are the T_g values measured by O-d.s.c. The solid line is the line fitted by the simple Gordon-Taylor equation, equation (21) from the measured T_g data. ΔT_2 is the difference between the measured and calculated T_g for the sample containing 34.6 wt.% NMP, whereas $\Delta T_{2'}$ is the difference for the sample containing 30.5 wt.% NMP

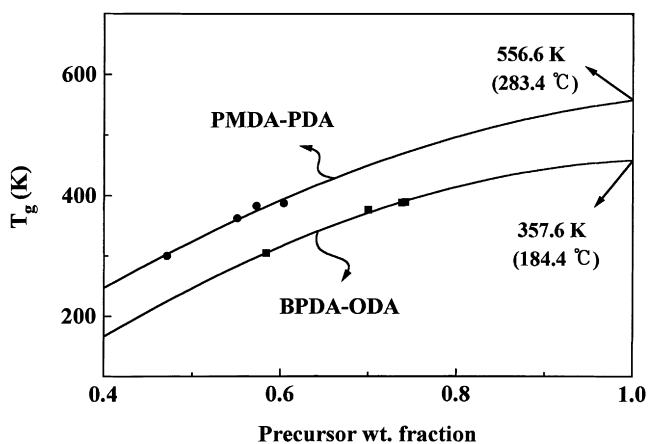


Figure 10 Variations of glass transition temperatures (T_g values) of PMDA-PDA precursor/NMP mixture and BPDA-ODA precursor/NMP mixture as a function of precursor weight fraction. The \blacksquare symbols denote the measured phase transition temperatures. The solid curves are the curves fitted by a modified Gordon-Taylor equation, equation (18) from the measured T_g data

the solvent-rich region (that is, *regime I*) T_g decreases linearly with increasing the precursor concentration until reaching to a critical concentration (W_c), which is perhaps related to the gel point, because the melting point (or freezing point) depression of NMP due to the dissolution of the poly(amic acid) with a high molecular weight. After reached to a critical concentration (W_c), the mixture gets into the precursor rich region (i.e. *regime II*), and T_g is inverted to increase with further increasing the precursor concentration. Consequently, for only the *regime II*, T_g increases convexly with varying composition. Thus, the modified Gordon-Taylor equation, equation (13) cannot be directly applicable for the entire compositions in the mixture of a poly(amic acid) and NMP solvent. That is, equation (13) can be applicable to the mixtures in only the *regime II*.

For the application of equation (14) to the precursor/NMP mixtures limited in the *regime II*, it was further modified in the following. In equation (13) the $\Delta\alpha_s$ and $T_{g,s}$ terms of the pure solvent are replaced by the $\Delta\alpha_c$ and $T_{g,c}$ terms of the mixture with the critical concentration W_c and the weight fractions (W_s and W_p) of solvent and precursor in a mixture are again fractionated by the $(1 - W_c)$ term rather than 1.0, which covers the entire concentration range, respectively:

$$T_g = \frac{\Delta\alpha_c T_{g,c} \left(\frac{1 - W_p}{1 - W_c} \right) + \Delta\alpha_p T_{g,p} \left(\frac{W_p - W_c}{1 - W_c} \right)}{\Delta\alpha_c \left(\frac{1 - W_p}{1 - W_c} \right) + \Delta\alpha_p \left(\frac{W_p - W_c}{1 - W_c} \right)} + \frac{\Delta k \left(\frac{1 - W_p}{1 - W_c} \right) \left(\frac{W_p - W_c}{1 - W_c} \right)}{\Delta\alpha_c \left(\frac{1 - W_p}{1 - W_c} \right) + \Delta\alpha_p \left(\frac{W_p - W_c}{1 - W_c} \right)} \quad (18)$$

where

$$W_c \leq W_p \leq 1.0 \quad (19)$$

and

$$\Delta\alpha_c = \Delta\alpha_s(1 - W_c) + \Delta\alpha_p W_c \quad (20)$$

$\Delta\alpha_s$ and $\Delta\alpha_p$ were calculated from the van der Waals volumes (V_w values)^{63,64} of the repeating unit of a precursor and the NMP solvent molecule, respectively, as described previously in the literature⁶⁵. The results are summarized in Tables 4 and 5.

In addition, for a given precursor/NMP system, Δk ($= k_g - k_r$) cannot be obtained conveniently. Thus, an estimate of Δk was attempted by analysing the T_g data measured for a precursor/NMP mixture with various compositions in the following manner. For the BPDA-PDA precursor/NMP mixture, four T_g data points in the *regime II* are plotted in Figure 9 as a function of the weight fraction of the precursor, and fitted by the simple Gordon-Taylor equation⁶², as shown below, using the lowest and highest T_g data points (namely, points 1 and 3 in Figure 9) as the reference T_g values:

$$T_g = \frac{\Delta\alpha_s T_{g,s} W_s + \Delta\alpha_p T_{g,p} W_p}{\Delta\alpha_s W_s + \Delta\alpha_p W_p} \quad (21)$$

In Figure 9, the two T_g points (that is, $T_{g,2}$ and $T_{g,2'}$) in the

intermediate region can be calculated by the following equations, respectively:

$$T_{g,2} = \frac{\Delta\alpha_1 T_{g,1}(W_3 - W_2) + \Delta\alpha_3 T_{g,3}(W_2 - W_1)}{\Delta\alpha_1(W_3 - W_2) + \Delta\alpha_3(W_2 - W_1)} \quad (22)$$

and

$$T_{g,2'} = \frac{\Delta\alpha_1 T_{g,1}(W_3 - W_{2'}) + \Delta\alpha_3 T_{g,3}(W_{2'} - W_1)}{\Delta\alpha_1(W_3 - W_{2'}) + \Delta\alpha_3(W_{2'} - W_1)} \quad (23)$$

where 1, 2, 2', and 3 denote the mixtures with four different weight fractions (W_1 , W_2 , $W_{2'}$, and W_3) of the precursor, respectively. Here, $\Delta\alpha_1$ and $\Delta\alpha_3$ are expressed below:

$$\Delta\alpha_1 = \Delta\alpha_s(1 - W_1) + \Delta\alpha_p W_1 \quad (24)$$

and

$$\Delta\alpha_3 = \Delta\alpha_s(1 - W_3) + \Delta\alpha_p W_3. \quad (25)$$

However, the measured $T_{g,2}$ and $T_{g,2'}$ are deviated by ΔT_2 and $\Delta T_{2'}$ from the T_g values calculated by equation (22) and equation (23), respectively, as shown in Figure 9. These deviations can be expressed by an equation in the following, as previously described for the modified Gordon–Taylor equation:

$$\Delta T_2 = \frac{\Delta k_2'(W_3 - W_2)(W_2 - W_1)}{\Delta\alpha_1(W_3 - W_2) + \Delta\alpha_3(W_2 - W_1)} \quad (26)$$

and

$$\Delta T_{2'} = \frac{\Delta k_2'(W_3 - W_{2'})(W_{2'} - W_1)}{\Delta\alpha_1(W_3 - W_{2'}) + \Delta\alpha_3(W_{2'} - W_1)}. \quad (27)$$

From these equations, $\Delta k_2'$ and $\Delta k_{2'}$ were calculated to be 0.012 and 0.017, respectively. The calculated $\Delta k_2'$ and $\Delta k_{2'}$ were averaged to give $\Delta k'$:

$$\Delta k' = \frac{\Delta k_2' + \Delta k_{2'}}{2} \quad (28)$$

The calculated $\Delta k_2'$ and $\Delta k_{2'}$ exhibit slightly different values, indicating that $\Delta k'$ is a function of the mixture composition. Thus, the $\Delta k'$ is normalized over the composition range (that is, $(W_3 - W_1)$) considered, and then further generalized for the regime II by multiplying $(1 - W_c)$, giving Δk :

$$\Delta k = \Delta k' \left(\frac{1 - W_c}{W_3 - W_1} \right) \quad (29)$$

$$= 0.106(1 - W_c). \quad (30)$$

Consequently, Δk is expressed as a function of the critical concentration (W_c). The parameters used in the estimation of Δk are listed in Table 4.

With the estimated Δk , T_g data measured for the BPDA-PDA precursor mixtures in the regime II were tried to be fitted by equation (18) with varying W_c . As shown in Figure 8, the best fitted result was obtained with $W_c = 0.521$, resulting in $T_g = 248.4^\circ\text{C}$ for the BPDA-PDA precursor in solvent free.

The Δk estimated for the BPDA-PDA precursor mixture was used to analyse of T_g data of the other precursor mixtures without further modification. For the PMDA-PDA precursor mixture, T_g values measured over the regime II were fitted by equation (18). The $W_c = 0.404$ gave the best result in the fitting (see Figure 10). The T_g of PMDA-PDA precursor without solvent was estimated to be

283.4°C . T_g values of the BPDA-ODA precursor mixtures were best fitted by equation (18) with $W_c = 0.505$, giving $T_g = 184.4^\circ\text{C}$ for the precursor in solvent free (see Figure 10). The T_g values of the precursors in solvent free are listed with the constants used for their estimations in Table 5.

Chain rigidities and their relationship to T_g values in poly(amic acid)s

In general, the chain rigidity of a polymer, which is known to play a critical role in the glass transition, is characterized by the statistical segment proposed by Kuhn⁶⁶, so-called Kuhn statistical segment. The Kuhn statistical segment (L_K) in a polymer chain is defined below:

$$L_K = \frac{\langle h^2 \rangle}{l} \quad (31)$$

$$= \frac{1}{\lambda} \frac{\langle h^2 \rangle}{n} \quad (32)$$

where $\langle h^2 \rangle$, l , and n are the mean square of end-to-end distance, the contour length (that is, the length of a fully extended chain), and the number of structural repeat units in a precursor polymer. λ is defined by l/n . Here, the mean square of end-to-end distance per a structural repeat unit, $\langle h^2 \rangle/n$ can be estimated by a method described by Birshtein and co-workers^{67,68}:

$$\frac{\langle h^2 \rangle}{n} = \sum_{\alpha=1}^v \sum_{\delta=0}^{v-1} \left[\frac{l_\alpha l_{[\alpha+\delta]} \{ \cos \gamma \}^\delta + (\cos \gamma)^{v-\delta}}{1 - (\cos \gamma)^v} \right] \quad (33)$$

with

$$[\alpha + \delta] : \alpha + \delta \quad \text{for } (\alpha + \delta) \leq v \quad \text{or} \\ \alpha + \delta - v \quad \text{for } (\alpha + \delta) > v. \quad (34)$$

Here, v , l_α , and $(\pi - \gamma)$ are the number of linear bonds in a structural repeating unit, the length of the α th bond, and the angle between the links, respectively.

Using equation (32) and equation (33) the Kuhn statistical segments of the precursor polymers considered were calculated in this study. The calculations were carried out with three assumptions in the following. First, the amide linkage in the repeat unit of a poly(amic acid) possesses a planar *trans*-structure⁶⁹. Second, in the poly(amic acid)s all the backbone skeletal valence angles, such as $\angle C_{ar}-C-N$, $\angle C-N-C_{ar}$, and $\angle C_{ar}-O-C_{ar}$ (see Figure 11), are equal to be 120° , as adapted previously by Birshtein *et al.*⁶⁷ in their calculations for polyimides. Finally, the precursors are alternatively linked by possible isomeric repeat units. For both BPDA-PDA and BPDA-ODA precursors, the chemical repeat units have four different isomeric structures as shown in Figure 11: *meta*-*para*, *meta*-*meta*, *para*-*para*, and *para*-*meta* isomers. The chemical repeat unit of PMDA-PDA precursor has two isomeric structures: *meta* and *para* isomers (see Figure 11).

The calculated results are listed in Table 6 with T_g values determined in the previous section. The calculated Kuhn statistical segment was 62.2 \AA for the BPDA-PDA precursor, 88.7 \AA for the PMDA-PDA precursor, and 41.2 \AA for the BPDA-ODA precursor. That is, the chain rigidity is in the increasing order BPDA-ODA < BPDA-PDA < PMDA-PDA. These chain rigidities are directly related to the T_g values. In comparison, the PMDA-PDA precursor with the highest chain rigidity exhibits the highest T_g ,

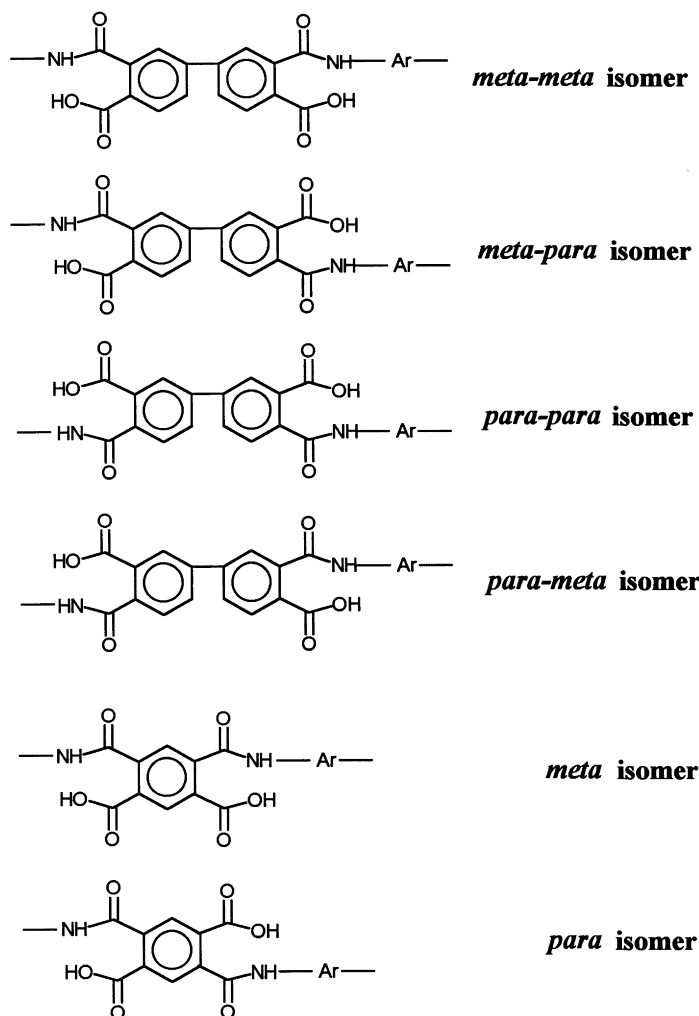


Figure 11 Possible isomeric repeat units in BPDA-PDA, BPDA-ODA, and PMDA-PDA precursors: Ar denotes PDA or ODA unit

Table 6 Kuhn statistical segments (L_K values) with their parameters and glass transition temperatures (T_g values) of several poly(amic acids) and polyamides

Polymers	ν	$\langle h^2 \rangle / n$ (\AA^2)	λ (\AA)	L_K (\AA)	T_g^a (K)
Precursors					
BPDA-PDA	4	3664.6	58.9	62.2	521.6
PMDA-PDA	1	1966.1	22.2	88.7	556.6
BPDA-ODA	8	3225.7	78.3	41.2	457.6
Polyamides					
i-PHA-BDA	1	867.0	14.7	58.9	558.0
i-PHA-PDA	1	491.5	11.1	44.3	500.0
i-PHA-ODA	1	253.9	8.0	31.9	463.0

^aGlass transition temperatures of polymers in solvent free

556.6 K (283.4°C), whereas the BPDA-ODA precursor with the lowest chain rigidity reveals the lowest T_g , 457.6 K (184.4°C). The BPDA-PDA precursor with an intermediate chain rigidity shows an intermediate T_g , 521.6 K (248.4°C).

The poly(amic acid)s studied in the present work can be classified into aromatic polyamides, because of their amide bond-based backbones. Thus, it is valuable to compare the determined chain rigidities and T_g values to those of aromatic polyamides, which have backbone structures similar to the precursor polymers, respectively. Here, three aromatic polyamides were considered in which T_g values were previously reported in the literature^{70–72}: poly(4,4'-biphenylene isophthalamide) (i-PHA-BDA),

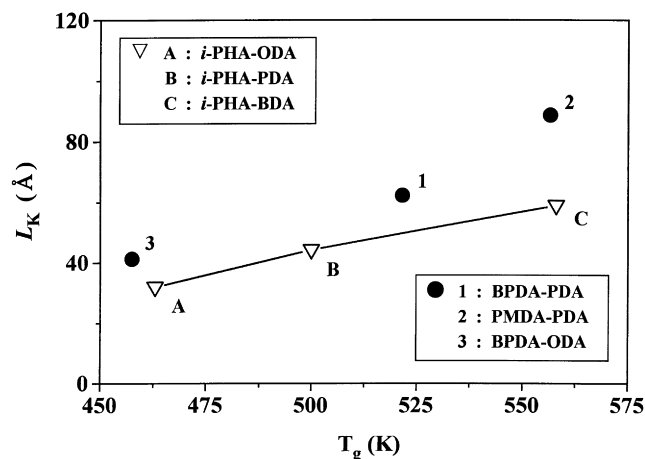


Figure 12 Relationships of Kuhn statistical segments (L_K values) and glass transition temperatures (T_g values) obtained for several aromatic poly(amic acid)s and polyamides

poly(*p*-phenylene isophthalamide) (i-PHA-PDA), and poly(4,4'-oxydiphenylene isophthalamide) (i-PHA-ODA). For these polyamides, Kuhn statistical segments were calculated in the same manner as described for the precursors. The calculated Kuhn statistical segments are compared with those of the precursors in Table 6 and

Figure 12. i-PHA-BDA exhibits $58.9 \text{ \AA } L_K$ and 558 K (285°C), whereas i-PHA-ODA reveals $31.9 \text{ \AA } L_K$ and 463 K (190°C). i-PHA-PDA shows $44.3 \text{ \AA } L_K$ and 500 K (227°C). For these polyamides, higher chain rigidity gives higher T_g . In comparison, i-PHA-BDA exhibits a chain rigidity slightly lower than that of BPDA-PDA precursor, but reveals higher T_g than that of BPDA-PDA by 36.4°C . The T_g of i-PHA-BDA is comparable with that of PMDA-PDA which has relatively much higher chain rigidity. i-PHA-ODA shows a chain rigidity lower than that of BPDA-ODA and, however, its T_g is slightly higher. i-PHA-PDA has a chain rigidity slightly higher than that of BPDA-ODA by only 3.1 \AA , but its T_g is higher than that of BPDA-ODA by 42.4°C . Overall, the poly(amic acid) precursors studied here exhibited relatively lower T_g than those of the polyamides considered, in spite of their relatively high chain rigidities. This result may result from two reasons in the following: First, all the poly(amic acid)s have two orthocarboxylic acid groups per a repeat unit, as side-groups. The side groups may cause a reduction of T_g . Second, the chain rigidities, which were calculated under the assumption that the precursors consist of their possible isomeric repeat units in the alternative manner, may be overestimated.

CONCLUSIONS

Three poly(amic acid) precursors were synthesized in aprotic NMP solvent from pairs of aromatic dianhydrides and diamines: BPDA-PDA, BPDA-ODA, and PMDA-PDA precursors. The precursor solutions were cast and then dried at various conditions. The amounts of residual NMP solvent in the dried precursor samples were determined by proton n.m.r. spectroscopy to be 25.8–88.3 wt.%, depending on the drying conditions. It is confirmed again in this study that the removal of all the NMP solvent from the cast poly(amic acid) samples is impossible because of the complexation between the solvent molecule and the orthoamic acid of the repeat unit in the precursors. From the n.m.r. spectroscopic results for the highly dried precursor samples, it is suggested that the chemical repeat unit in a poly(amic acid) complexes with 1.46–2.16 NMP molecules, depending on the precursors.

For samples of the poly(amic acid)s dried at various conditions, T_g values were successfully measured by the new oscillating d.s.c. technique, which was recently developed, as a function of the content of residual NMP solvent. Furthermore, for the precursor/NMP mixtures, phase diagrams were constructed from the T_g values measured with varying compositions. In addition, T_g values of the precursors in solvent free (namely, true T_g values of the precursors) were estimated by fitting the measured T_g values by a modified Gordon–Taylor equation as a function of composition: 248.4°C for BPDA-PDA, 283.4°C for PMDA-PDA, and 184.4°C for BPDA-ODA precursor.

The Kuhn statistical segment, which is a measure of chain rigidity, was calculated for the precursor polymers as well as some selected polyamides which have backbone structures similar to the precursors. Overall, higher chain rigidity causes higher T_g for both the precursors and the polyamides. In comparison to the polyamides, the precursors exhibited relatively low T_g values in spite of the relatively high chain rigidities. This may result from two reasons: (i) the orthocarboxylic acid groups in the precursors may reduce T_g values; and (ii) the chain rigidities calculated in the precursors may be overestimated.

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